<table>
<thead>
<tr>
<th>Page</th>
<th>Location</th>
<th>Instead of</th>
<th>Correction</th>
</tr>
</thead>
<tbody>
<tr>
<td>4-14</td>
<td>Section 4.9.4, first line in first paragraph</td>
<td>resistance</td>
<td>resistance</td>
</tr>
<tr>
<td>AI-2</td>
<td>Symbol for Slip relaxation constant</td>
<td>$K_l$</td>
<td>$K_l$</td>
</tr>
<tr>
<td>AI-2</td>
<td>Symbol for Panel length</td>
<td>$l$</td>
<td>$l$</td>
</tr>
<tr>
<td>AI-2</td>
<td>Symbol for Purlin or joist spacing</td>
<td>$v$</td>
<td>$v$</td>
</tr>
<tr>
<td>AI-2</td>
<td>Symbol for Resisting shear couples at panel ends and purlins</td>
<td>$M_e, M_o$</td>
<td>$M_e, M_p$</td>
</tr>
</tbody>
</table>

**AI-19 LRFD column**

$S_w = 2132 \text{plf} \ldots \phi S_w = 0.80 \times 2132 \text{plf} = 1706 \text{plf} \{24.88 \text{kN/m}\}$

$S_n = 1425 \text{plf} \ldots \phi S_n = 0.80 \times 1425 \text{plf} = 1140 \text{plf} \{16.63 \text{kN/m}\}$

**AI-19 ASD column**

$S_w/\Omega = 2132/2.00 = 1066 \text{plf} \{15.55 \text{kN/m}\}$

$S_n/\Omega = 1425/2.00 = 713 \text{plf} \{10.40 \text{kN/m}\}$

**AI-25 Top LRFD column**

$\phi S_w = 0.80 \times 2130 \text{plf} = 1704 \text{plf} \{24.86 \text{kN/m}\}$

$\phi S_n = 0.80 \times 2050 \text{plf} = 1640 \text{plf} \{23.93 \text{kN/m}\}$

**AI-25 Top ASD column**

$S_w/\Omega = 2130/2.00 = 1065 \text{plf} \{15.54 \text{kN/m}\}$

$S_n/\Omega = 2050/2.00 = 1025 \text{plf} \{14.96 \text{kN/m}\}$

**AI-25 Paragraph**

"To calculate the stiffness of the diaphragm,..." $D_{xx} = 39.3 \text{mm}$ $D_{xx} = 39 \text{m}$

**AI-29 ASD portion**

(See Appendix All, page AI-21) (See Appendix All, page AI-23)

**AI-35 First paragraph**

"...on a 24/8 connection pattern will be used which is..." "...on a 24/8 connection pattern will be used, which is..."

**AI-71 First paragraph**

"...considering possible use of 3/4in. {19mm} shear studs..." "...considering possible use of 3/4in. {19mm} shear studs..."

**AI-73 Second LRFD/ASD portion**

"...and meet the required spacing. However, ..." "...and meet the required spacing. However, ...

**AIV-12 Heading of Table VII, Table VII-M, Table VIII, Table VIII-M**

Add $\phi_u = 0.5 \Omega_u = 3.0$, (same as to Table VI and VI-M)

**AIV-13 Heading of Table IX, Table IX-M**

Add $\phi_u = 0.5 \Omega_u = 3.0$, (same as to Table VI and VI-M)

**AIV-13 Table IX, X-EDN19/X-EDNK22 column**

1369, 1813 and 2287

1298, 1719 and 2168 respectively

**AIV-13 Table IX-M, X-EDN19/X-EDNK22 column**

6.09, 8.06 and 10.17

5.77, 7.65 and 9.65 respectively

**AV-3 Second paragraph from the bottom**

"(rigid insulating boards should be held 3 in. away from...)

"(rigid insulating boards should be held 3 ft away from...)

November 2006