

The following excerpt are pages from the North American Product Technical Guide, Volume 2: Anchor Fastening, Edition 21.

Please refer to the publication in its entirety for complete details on this product including data development, product specifications, general suitability, installation, corrosion and spacing and edge distance guidelines.

US&CA: https://submittals.us.hilti.com/PTGVol2/

To consult directly with a team member regarding our anchor fastening products, contact Hilti's team of technical support specialists between the hours of 7:00am – 6:00pm CST.

US: 877-749-6337 or <u>HNATechnicalServices@hilti.com</u>

CA: 1-800-363-4458, ext. 6 or CATechnicalServices@hilti.com



3.3.17 KCS-WF CAST-IN ANCHOR

PRODUCT DESCRIPTION

KCS-WF cast-in anchors

Anchor System Feature Instruction KCS-WF internally threaded cast-in anchors for wood KCS-WF internally threaded cast-in anchors for wood KCS-WF internally threaded cast-in anchors for wood KCS-WF internally threaded cast-in anchors for wood

Features and Benefits

- Installation performed on top of the formwork. No overhead drilling. No scissor lift rental
- Hexagonal head prevents spinning in concrete
- Anchor bodies are color coded for quick identification
- KCS-WF have large plastic flanges for secure seating to wood form. This prevents concrete seepage into the threading.
- KCS-WF have notched nails that snap off easily at the concrete surface after the wood forms are stripped.









Uncracked concrete

Cracked concrete

Seismic design categories A-F

Fire Sprinkler Listings

Approvals/Listings	
ICC-ES (International Code Council)	ESR-4006 in concrete per ACI 318 Ch. 17 / ICC-ES AC446
2015 International Building Code / International Residential Code (IBC/IRC)	
City of Los Angeles	RR 26069
FM (Factory Mutual)	Pipe hanger components for automatic sprinkler systems for 3/8 through 3/4
Florida Building Code	2017 FBC Supplement (within ESR-4006)
UL LLC (Underwriters Laboratory LLC)	Pipe hanger equipment for fire protection services for 3/8 through 3/4









MATERIAL SPECIFICATIONS

Component	KCS-WF
Insert body	Heat treated carbon steel
Flange	Engineered plastic
Spring	N/A
Plating	Zinc clear chromate plating
Protective sleeve	N/A

Table 1 — Hilti KCS-WF specification table

Satting information	Symbol	Units	Nominal anchor diameter						
Setting information	Symbol	Units	1/4	3/8	1/2	5/8	3/4		
Insert thread	d	UNC	1/4-20	3/8-16	1/2-13	5/8-11	3/4-10		
Minimum thread angagement	0	in.	1/4	3/8	1/2	5/8	3/4		
Minimum thread engagement	ℓ_{th}	(mm)	(6)	(10)	(13)	(16)	(19)		
Diagtic flance diameter	А	in.	1.33	1.33	1-1/2	1.60	1-2/3		
Plastic flange diameter	d _{pf}	(mm)	(33)	(33)	(38)	(41)	(43)		
Diagtic flangs thickness		in.	.11	.11	.11	.11	.11		
Plastic flange thickness	t _{pf}	(mm)	(2.8)	(2.8)	(2.8)	(2.8)	(2.8)		
Lanath	ℓ	in.	1-1/4	1-1/4	1-3/4	2.14	2.14		
Length	· ·	(mm)	(32)	(32)	(45)	(54)	(54)		
Steel head thickness		in.	1/8	1/8	1/8	.14	.14		
Steer nead thickness	t _{sh}	(mm)	(3.3)	(3.3)	(3.1)	(3.5)	(3.5)		
Langth of brook off poils	,	in.	1	1	1	3/4	3/4		
Length of break-off nails	ℓ_{n}	(mm)	(24.4)	(24.4)	(23.5)	(19.0)	(19.0)		
Minimum alab thialman	h	in.	2-1/2	2-1/2	2-1/2	3-3/4	3-3/4		
Minimum slab thickness	h	(mm)	(64)	(64)	(64)	(95)	(95)		

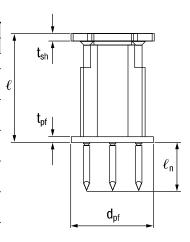


Figure 1 — KCS-WF specifications

DESIGN INFORMATION IN CONCRETE PER ACI 318

ACI 318 Chapter 17

The technical data contained in this section are Hilti Simplified Design Tables. The load values were developed using the Strength Design parameters and variables of ESR-4006 and the equations within ACI 318 Chapter 17. For a detailed explanation of the Hilti Simplified Design Tables, refer to section 3.1.8. Data tables from ESR-4006 are not contained in this section, but can be found at www.icc-es.org or at www.hilti.com.

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Table 2 — Hilti KCS-WF cast-in insert design strength with concrete/pullout failure in uncracked concrete 1,2,3,4,5

Nominal			Tensio	n - фN _п		Shear - φV _n				
anchor internal diameter in.	Effective embed. depth in. (mm)	f' = 2,500 psi (17.2 MPa) lb (kN)	f' = 3,000 psi (20.7 MPa) lb (kN)	f' = 4,000 psi (27.6 MPa) lb (kN)	f' = 6,000 psi (41.1 MPa) lb (kN)	f' = 2,500 psi (17.2 MPa) lb (kN)	f' = 3,000 psi (20.7 MPa) lb (kN)	f' = 4,000 psi (27.6 MPa) lb (kN)	f' = 6,000 psi (41.1 MPa) lb (kN)	
1/4	1.11	1,230	1,350	1,560	1,910	1,230	1,350	1,560	1,910	
and 3/8	(28)	(5.5)	(6.0)	(6.9)	(8.5)	(5.5)	(6.0)	(6.9)	(8.5)	
1/2	1.63	2,190	2,400	2,770	3,395	2,190	2,400	2,770	3,395	
	(42)	(9.7)	(10.7)	(12.3)	(15.1)	(9.7)	(10.7)	(12.3)	(15.1)	
E /0	1.90	2,750	3,015	3,480	4,265	2,750	3,015	3,480	4,265	
5/8	(48)	(12.2)	(13.4)	(15.5)	(19.0)	(12.2)	(13.4)	(15.5)	(19.0)	
2/4	1.83	2,590	2,835	3,275	4,015	2,590	2,835	3,275	4,015	
3/4	(46)	(11.5)	(12.6)	(14.6)	(17.9)	(11.5)	(12.6)	(14.6)	(17.9)	

Table 3 — Hilti KCS-WF cast-in insert design strength with concrete/pullout failure in cracked concrete 1.2.3.4.5

Nominal			Tensio	n - фN _n		Shear - φV _n				
anchor internal diameter in.	Effective embed. depth in. (mm)	f' = 2,500 psi (17.2 MPa) lb (kN)	f' = 3,000 psi (20.7 MPa) lb (kN)	f' = 4,000 psi (27.6 MPa) lb (kN)	f' = 6,000 psi (41.1 MPa) lb (kN)	f' _c = 2,500 psi (17.2 MPa) lb (kN)	f' = 3,000 psi (20.7 MPa) lb (kN)	f' = 4,000 psi (27.6 MPa) Ib (kN)	f' = 6,000 psi (41.1 MPa) lb (kN)	
1/4	1.11	985	1,080	1,245	1,530	985	1,080	1,245	1,530	
and 3/8	(28)	(4.4)	(4.8)	(5.5)	(6.8)	(4.4)	(4.8)	(5.5)	(6.8)	
1 /0	1.63	1,750	1,920	2,215	2,715	1,750	1,920	2,215	2,715	
1/2	(42)	(7.8)	(8.5)	(9.9)	(12.1)	(7.8)	(8.5)	(9.9)	(12.1)	
E /0	1.90	2,200	2,410	2,785	3,410	2,200	2,410	2,785	3,410	
5/8	(48)	(9.8)	(10.7)	(12.4)	(15.2)	(9.8)	(10.7)	(12.4)	(15.2)	
2 /4	1.83	2,070	2,270	2,620	3,210	2,070	2,270	2,620	3,210	
3/4	(46)	(9.2)	(10.1)	(11.7)	(14.3)	(9.2)	(10.1)	(11.7)	(14.3)	

¹ See section 3.1.8 to convert design strength value to ASD value.

² Linear interpolation between concrete compressive strengths is not permitted.

³ Tabular values are for single anchor located at edge distance (c) and spacing (s) greater than 3h_{et}. For anchors with edge distance or spacing less than 3h_{et} use ACI 318 to calculate load reduction factor. Compare the value to the steel values in Table 11. The lesser of the values is to be used for the design.

⁴ Tabular values are for normal-weight concrete only. For lightweight concrete multiply design strength by λ_a as follows: for sand-lightweight, $\lambda_a = 0.85$; for all-lightweight, $\lambda_a = 0.75$

⁵ Tabular values are for static loads only. Seismic design is not permitted for uncracked concrete. For seismic tension loads, multiply cracked concrete tabular values in tension by α_{N.seis} = 0.75. No reduction needed for seismic shear.

Table 4 — Design strength for steel failure of common threaded rods and KCS-WF inserts¹

	Grade A36 threaded rod				93 B7 or ASTM 105 threaded roo	KCS-WF insert		
	Tensile ²			Tensile ²			Tensile	Shear
Nominal	φN _{sa,rod}		Seismic	φN _{sa,rod}		Seismic	φN _{sa,insert}	φV _{sa,insert}
anchor	or	Shear ³	shear⁴	or	Shear ³	shear⁴	or	or
diameter in.	φΝ _{sa,eq,rod} lb (kN)	φV _{sa,rod} lb (kN)	φV _{sa,eq,rod} Ib (kN)	φΝ _{sa,eq,rod} Ib (kN)	φV _{sa,rod} Ib (kN)	φV _{sa,eq,rod} Ib (kN)	φΝ _{sa,eq,insert} Ib (kN)	φV _{sa,eq,insert} Ib (kN)
1/4	1,390	720	505	3,000	1,550	1,085	2,450	1,650
1/4	(6.2)	(3.2)	(2.2)	(13.3)	(6.9)	(4.8)	(10.9)	(7.3)
0./0	3,395	1,750	1,225	7,315	3,780	2,646	2,450	1,650
3/8	(15.1)	(7.8)	(5.4)	(32.5)	(16.8)	(11.8)	(10.9)	(7.3)
1 /0	6,175	3,210	2,245	13,315	6,915	4,841	8,465	2,110
1/2	(27.5)	(14.3)	(10.0)	(59.2)	(30.8)	(21.5)	(37.7)	(9.4)
F /0	9,835	5,110	3,575	21,190	11,020	7,714	9,100	5,215
5/8	(43.7)	(22.7)	(15.9)	(94.3)	(49.0)	(34.3)	(40.5)	(23.2)
0.74	14,550	7,565	5,295	31,405	16,305	11,414	9,100	5,440
3/4	(64.7)	(33.7)	(23.6)	(139.7)	(72.5)	(50.8)	(40.5)	(24.2)

See section 3.1.8 to convert design strength value to ASD value.

Table 5 — UL LLC and FM approvals^{1,2}

	• •									
Nominal	KCS-WF									
anchor diameter in.	UL max pipe size (in.)	UL test load (lb)	FM max pipe size (in.)							
3/8	4	1,500	4							
1/2	8	4,050	8							
5/8	8	4,050	-							
3/4	8	4,050	-							

UL LLC Listing based on successful completion of testing in accordance with UL 203.
 FM Approval based on successful completion of testing in accordance with FM 1952.

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Tensile values determined by static tension tests with ϕ N $_{sa} = \phi A_{gs,N}$ f_{uta} as noted in ACI 318 Chapter 17. Shear values determined by static shear tests with ϕ V $_{sa} = \phi$ 0.60 $A_{gs,V}$ f_{uta} as noted in ACI 318 Chapter 17. Seismic shear values determined by seismic shear tests with ϕ V $_{sa} \le \phi$ 0.60 $A_{gs,V}$ f_{uta} as noted in ACI 318 Chapter 17.



DESIGN INFORMATION IN CONCRETE PER CSA A23.3

Limit State Design of anchors is described in the provisions of CSA A23.3 Annex D for post-installed anchors tested and assessed in accordance with ACI 355.2 for mechanical anchors and ACI 355.4 for adhesive anchors. This section contains the Limit State Design tables with unfactored characteristic loads that are based on the published loads in ICC Evaluation Services ESR-4006. These tables are followed by factored resistance tables. The factored resistance tables have characteristic design loads that are prefactored by the applicable reduction factors for a single anchor with no anchor-to-anchor spacing or edge distance adjustments for the convenience of the user of this document. All the figures in the previous ACI 318 Chapter 17 design section are applicable to Limit State Design and the tables will reference these figures.

For a detailed explanation of the tables developed in accordance with CSA A23.3 Annex D, refer to Section 3.1.8. Technical assistance is available by contacting Hilti Canada at (800) 363-4458 or at www.hilti.com.

Table 6 — Hilti KCS-WF design information in accordance with CSA A23.3 Annex D1



	dance wit	th GOA ALGIG Allifox B						
Docime novements:	Cumahad	Lluita	Nominal anchor diameter					Ref
Design parameter	Symbol	Units	1/4	3/8	1/2	5/8	3/4	A23.3-04
Analog O D		in.	0.51		0.67	0.87	1	
Anchor O.D.	d _a	(mm)	(13)		(17)	(22)	(25)	
Effective explored exect		in.	1.	11	1.63	1.9	1.83	
Effective embedment	h _{ef}	(mm)	(2	28)	(41)	(48)	(46)	
Minimum annual deinimum	la la	in.		2-1/2	,	3-	3/4	
Minimum concrete thickness	h _{min}	(mm)		(64)		(9	95)	
Minimum edge distance		in.			1-1/2	•		
Willimum edge distance	C _{min}	(mm)			(38)			
Minimum anchor spacing		in.	2.	04	2.68	3.48	4.00	
William anchor spacing	S _{min,untor}	(mm)	(5	52)	(68)	(88)	(102)	
Steel embed. material resistance factor for reinforcement	φ _s	-			0.85	-		8.4.3
Resistance modification factor for tension, steel failure modes ²	R	-			0.70			D.5.3
Resistance modification factor for shear, steel failure modes ²	R	-	0.65					
Factored at all registers of interesting	N.	lb	2,243	2,243	7,747	8,330	8,330	D.6.1.2
Factored steel resistance in tension	N _{sar}	(kN)	(10.0)	(10.0)	(34.4)	(37.0)	(37.0)	D.0.1.2
Factored steel resistance in tension	N	lb	2,243	2,243	7,747	8,330	8,330	D.6.1.2
Tactored steel resistance in tension	N _{sar, eq}	(kN)	(10.0)	(10.0)	(34.4)	(37.0)	(37.0)	D.0.1.2
Factored steel resistance in shear	V _{sar}	lb	1,519	1,519	1,945	4,801	5,011	D.7.1.2
Tactored steel resistance in snear	sar	(kN)	(6.8)	(6.8)	(8.6)	(21.3)	(22.3)	D.7.1.2
Factored steel resistance in shear, seismic	l v	lb	1,519	1,519	1,945	4,801	5,011	D.7.1.2
·	V _{sar,eq}	(kN)	(6.8)	(6.8)	(8.6)	(21.3)	(22.3)	D.7.11.2
Coeff. for factored conc. breakout resistance, uncracked concrete	k _{c,uncr}	-	10			D.6.2.2		
Coeff. for factored conc. breakout resistance, cracked concrete	k _{c,cr}	-			10			D.6.2.2
Modification factor for anchor resistance, tension, uncracked conc.	$\Psi_{c,N}$	-	1.25			D.6.2.6		
Modification factor for anchor resistance, tension, cracked conc.	$\Psi_{c,N}$	-	1.0			D.6.2.6		
Anchor category	-	-	Cast-in			D.5.3 (c)		
Concrete material resistance factor	Фс	-			0.65			8.4.2
Resistance modification factor for tension and shear, concrete failure modes, Condition B ³	R	-	1.00				D.5.3 (c)	

¹ Design information in this table is taken from ICC-ES ESR-4006, dated 11/2017, tables 1 and 3, and converted for use with CSA A23.3 (R2014) Annex D.

² The carbon steel KCS-WF is considered a brittle steel element as defined by CSA A23.3 (R2014) Annex D section D.2.

³ For use with the load combinations of CSA A23.3 (R2014) chapter 8. Condition B applies where supplementary reinforcement in conformance with CSA A23.3 (R2014) section D.5.3 is not provided, or where pullout or pryout strength governs. For cases where the presence of supplementary reinforcement can be verified, the resistance modification factors associated with Condition A may be used.

Table 7 — Hilti KCS-WF cast-in insert design strength with concrete / pullout failure in uncracked concrete 1.2.3.4.5

Nominal				Tensio	on - N _r		Shear - V _r			
anchor	Effective	Nominal	f' = 20 MPa	f' = 25 MPa	f' = 30 MPa	f' = 40 MPa	$f'_{c} = 20 \text{ MPa}$	$f'_{c} = 25 \text{ MPa}$	f' = 30 MPa	$f'_{c} = 40 \text{ MPa}$
diameter	embed.	embed.	(2,900psi)	(3,625 psi)	(4,350 psi)	(5,800 psi)	(2,900 psi)	(3,625 psi)	(4,350 psi)	(5,800 psi)
in.	in. (mm)	in. (mm)	lb (kN)	lb (kN)	lb (kN)	lb (kN)	lb (kN)	lb (kN)	lb (kN)	lb (kN)
1/4 and	1.11	1.18	1,230	1,375	1,505	1,740	1,230	1,375	1,505	1,740
3/8	(28)	(30)	(5.5)	(6.1)	(6.7)	(7.7)	(5.5)	(6.1)	(6.7)	(7.7)
1/2	1.63	1.81	2,185	2,440	2,675	3,090	2,185	2,440	2,675	3,090
1/2	(42)	(46)	(9.7)	(10.9)	(11.9)	(13.8)	(9.7)	(10.9)	(11.9)	(13.8)
5/8	1.90	2.24	2,740	3,065	3,360	3,880	2,740	3,065	3,360	3,880
	(48)	(57)	(12.2)	(13.6)	(15.0)	(17.3)	(12.2)	(13.6)	(15.0)	(17.3)
3/4	1.83	2.24	2,580	2,885	3,160	3,650	2,580	2,885	3,160	3,650
	(46)	(57)	(11.5)	(12.8)	(14.1)	(16.2)	(11.5)	(12.8)	(14.1)	(16.2)

Table 8 — Hilti KCS-WF cast-in insert design strength with concrete / pullout failure in cracked concrete 1.2.3.4.5

Table 0	able 0 — This 100-Wi Gast-in insert design strength with concrete / pundit failure in cracked concrete									
Nominal				Tensio	on - N _r		Shear - V _r			
anchor	Effective	Nominal	f' = 20 MPa	f' c = 25 MPa	$f'_{c} = 30 \text{ MPa}$	$f'_{c} = 40 \text{ MPa}$	f' c = 20 MPa	$f'_{c} = 25 \text{ MPa}$	$f'_{c} = 30 \text{ MPa}$	$f'_{c} = 40 \text{ MPa}$
diameter	embed.	embed.	(2,900psi)	(3,625 psi)	(4,350 psi)	(5,800 psi)	(2,900 psi)	(3,625 psi)	(4,350 psi)	(5,800 psi)
in.	in. (mm)	in. (mm)	lb (kN)	lb (kN)	lb (kN)	lb (kN)	lb (kN)	lb (kN)	lb (kN)	lb (kN)
1/4 and	1.11	1.18	985	1,100	1,205	1,390	985	1,100	1,205	1,390
3/8	(28)	(30)	(4.4)	(4.9)	(5.4)	(6.2)	(4.4)	(4.9)	(5.4)	(6.2)
1/2	1.63	1.81	1,745	1,955	2,140	2,470	1,745	1,955	2,140	2,470
1/2	(42)	(46)	(7.8)	(8.7)	(9.5)	(11.0)	(7.8)	(8.7)	(9.5)	(11.0)
5/8	1.90	2.24	2,195	2,455	2,685	3,100	2,195	2,455	2,685	3,100
5/6	(48)	(57)	(9.8)	(10.9)	(11.9)	(13.8)	(9.8)	(10.9)	(11.9)	(13.8)
2//	1.83	2.24	2,065	2,310	2,530	2,920	2,065	2,310	2,530	2,920
3/4	(46)	(57)	(9.2)	(10.3)	(11.3)	(13.0)	(9.2)	(10.3)	(11.3)	(13.0)

See section 3.1.8 to convert factored resistance value to ASD value.

INSTALLATION INSTRUCTIONS

Installation Instructions For Use (IFU) are included with each product package. They can also be viewed or downloaded online at www.hilti.com. Because of the possibility of changes, always verify that downloaded IFU are current when used. Proper installation is critical to achieve full performance. Training is available on request. Contact Hilti Technical Services for applications and conditions not addressed in the IFU.

ORDERING INFORMATION¹

KCS - WF cast-in anchor for use in wood forms

	Sleeve	
Description	color ²	Qty / box
KCS - WF 1/4	Green	150
KCS - WF 3/8	Red	150
KCS - WF 1/2	Orange	100
KCS - WF 5/8	Yellow	100
KCS - WF 3/4	Black	100

3.3.17

Linear interpolation between concrete compressive strengths is not permitted.

Tabular values are for single anchor located at edge distance (c) and spacing (s) greater than 3h_{ef}. For anchors with edge distance or spacing less than 3h_{ef} use CSA A23.3 to calculate load reduction factor. Compare the value to the steel values in Table 23. The lesser of the values is to be used for the design.

⁴ Tablular values are for normal weight concrete only. For lightweight concrete multiply design strength by λ_a as follows:

For sand-lightweight, $\lambda_a = 0.85$; for all-lightweight, $\lambda_a = 0.75$.

⁵ Tabular values are for static loads only. Seismic design is not permitted for uncracked concrete. For seismic loads, multiply cracked concrete tabular values by $\alpha_{\rm sec} = 0.75$.